

TRANSMITTAL

To: Mr. Bob Griffis
Utility Trailer Manufacturing Company
17295 East Railroad Street
City of Industry, California 91749

From: Kurt Wiebe *(KW)*

Date: February 10, 1994

Subject: Draft Interim Remedial Action Plan

Project Number: 26961 2

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Attached is Harding Lawson Associates' (HLA) *Draft Interim Remedial Action Plan, Soil-vapor Extraction, Utility Trailer Manufacturing Company, 17300 East Chestnut Street, City of Industry, California.* Please call Brad Eismen or me at (714) 556-7992 if you have any questions or comments.



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UTM 004561

**Draft Interim Remedial Action Plan
Soil-Vapor Extraction
Utility Trailer Manufacturing Company
17300 East Chestnut Street
City of Industry, California**

Prepared for

Utility Trailer Manufacturing Company
17295 East Railroad Street
City of Industry, California 91749

HLA Project No. 26961 2

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UTM 004562

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1.0 INTRODUCTION

This document presents the interim remedial action plan (IRAP) for soil-vapor extraction (SVE) at Utility Trailer Manufacturing Company (UTM), located at 17300 East Chestnut Street, City of Industry, California. This IRAP has been developed at the request of Messrs Philip Chandler and Samuel Yu of the Regional Water Quality Control Board-Los Angeles Region (RWQCB), at a meeting attended by representatives of UTM and HLA on November 15, 1993. This IRAP provides the objectives, technical approach, and proposed implementation schedule for the remediation of halogenated volatile organic compound (VOC)-affected soil at the site.

Harding Lawson Associates (HLA) performed in-situ vapor extraction testing in October 1993, as part of a Phase II site assessment. Results of this testing yielded favorable results in both zones tested. Test results are detailed in HLA's report entitled *Phase II Site Assessment, Utility Trailer Manufacturing Company, 17300 East Chestnut Street, City of Industry, California*, dated December 1, 1993 (HLA, 1993d). Based on these results, soil-vapor extraction (SVE) is proposed as an interim remedial measure for soil cleanup at the three affected areas of the site.

This proposed interim remedial action is intended to document the most appropriate and feasible technology available to achieve the following goals:

- Protect groundwater from possible impact by the elevated concentrations of the compounds of concern (COCs) reported in the soil matrix.
- Reduce the concentrations of the COCs in the soil vapor and matrix to acceptable operational levels as discussed in the November 15, 1993, meeting.
- Use a phased approach to implement the remedial action, beginning with subareas of the three main areas, which indicate the highest concentrations of halogenated VOCs reported in soil matrix and soil-vapor samples collected during Phase II site assessment activities. The remaining subareas will be addressed once the effectiveness of these remedial efforts is demonstrated and is approved by the RWQCB.
- Conduct all field activities in a safe and efficient manner.

2.0 BACKGROUND

2.1 Site Description

The site is located between Railroad and East Chestnut Streets, south of Azusa Avenue, in the City of Industry, California (Plate 1). The site is bounded on the north by Chestnut Street and San Jose Creek and on the west by a field adjacent to Azusa Avenue. Somitex Prints of California (Somitex), the Los Angeles Water Company (LA Water), and Maxim Lighting abut the southern and eastern boundaries of the site. The main manufacturing building, plant operations building, numerous small operational support buildings, and a quality assurance test track are currently located on the site. The property is paved with asphalt and concrete, except for two unpaved areas located on the northern and western portions of the property.

The approximately 27-acre site is situated in the Puente Valley, with the San Jose Hills to the north and the Puente Hills to the south, at an approximate elevation of 380 feet above Mean Sea Level (MSL). The Puente Valley is the southernmost tributary valley of the larger San Gabriel Valley. Site terrain is generally flat, sloping gently to the north toward San Jose Creek. San Jose Creek originates approximately 30 miles upstream of the UTM site, runs past UTM, and then flows into the San Gabriel River at Whittier Narrows, approximately 6 miles downstream of the site.

2.2 Geology

The site lies within the Northeastern structural block of the Peninsular Range physiographic province (Yerkes et al., 1965). The Puente Valley is a structural basin filled with Quaternary alluvial deposits and underlain by Tertiary sedimentary rocks. The Tertiary-age sequence consists of fine- to coarse-grained marine clastic sedimentary rocks and has been divided into three formational units, the Puente, Repetto, and Pico formations (oldest to youngest, respectively). Quaternary sediments consist of unconsolidated to semiconsolidated alluvial and terrace deposits. The surficial alluvium is probably 300 to 400 feet thick beneath the site (Mann, 1986).

Investigations conducted at the site indicate that the site is underlain by alluvial deposits consisting of interbedded clay, silt, sand, and gravel. Sediments from the ground surface to approximately 15 feet below ground surface (bgs) consist of very stiff clay. This upper clay unit tends to be thicker on the southern portion of the site. Below this, to a depth of approximately 20 to 30 feet bgs, is an interval of interbedded silty sand, fine-grained sand, clayey sand, and silt (uppermost sand). Beneath this zone, to a depth of approximately 35 to 45 feet bgs, is an interval of fine- to coarse-grained sand and fine to coarse gravel.

2.3 Hydrogeology

The site is located within the Puente Groundwater Basin, a subbasin of the larger San Gabriel Valley Groundwater Basin. Groundwater flows into the Puente Basin through a gap at the northeastern end of the basin (Department of Water Resources [DWR], 1966). Groundwater flow in the basin is westerly, generally parallel to San Jose Creek, and flows out of the basin at Whittier Narrows. The principal water-bearing formations of the Puente Basin are the upper members of the Pico Formation and the Older and Younger Alluvium. Borings drilled at the site encountered groundwater at a depth of approximately 22 feet bgs. Depth to the base of fresh water is estimated to be approximately 200 feet bgs at the site (DWR, 1966).

2.4 Previous Investigations

A summary of investigations conducted at the site is included in the HLA report entitled, *Site Assessment, Utility Trailer Manufacturing Company, 17300 East Chestnut Street, City of Industry, California*, dated December 23, 1992 (HLA, 1992e; HLA, 1993d). These investigations have identified three general areas that contain elevated concentrations of halogenated VOCs in soil-gas and soil-matrix samples. These areas include the area near the northern end of the drainage conduit from Somitex (North Area), an area located at the southern end of the drainage conduit (Southwest Area), and an area near the former solvent storage location at the southeastern portion of the facility (Southeast Area). The predominant VOCs previously reported from soil-gas and soil-matrix samples at the site are 1,1-dichloroethene (1,1-DCE), 1,1,1-trichloroethane (1,1,1-TCA), tetrachloroethene (PCE), and trichloroethene (TCE).

The soil-vapor extraction testing conducted in the North area during the Phase II site assessment indicated that SVE is a technically viable approach to remove halogenated VOCs from both the upper clay zone and the uppermost sand zone. Propagated vacuums at most upper clay zone piezometers showed a slow rise throughout the test and indicated that a vacuum of 1 inch of water was propagated to a radius of approximately 9 feet from the vapor extraction well in that zone after approximately 7 hours. Propagated vacuums in most uppermost sand zone piezometers appeared to have stabilized by the end of the test and indicated that a vacuum of 1 inch of water was propagated to a radius greater than 25 feet from the vapor extraction well in that zone after approximately 7 hours. Approximately 1 gallon of dense nonaqueous phase liquid (DNAPL) and approximately 5 gallons of water were recovered from the vapor extraction system condenser during each test. Analytical results of the DNAPL indicated a makeup of predominantly PCE with lesser amounts of TCE (approximately 81 percent PCE and 4 percent TCE in the upper clay zone and approximately 91 percent PCE and 2 percent TCE in the uppermost sand zone).

2.5 Lithologic Controls

Based on an aerial photograph review performed as part of a Phase I site assessment (HLA, 1992b), the site area was predominantly used for agricultural cultivation and the raising of livestock through at least 1954. The presence of lithologic features (calcified stringers, root holes, and worm tubes) in the upper clay zone are likely related to these activities. These features have probably influenced the migration of contaminants and will likewise probably influence remediation of this zone. These features are likely the reason for the relatively high propagated vacuums and radius of influence measured during the vapor extraction test of this zone.

Total organic carbon (TOC) analyses performed on selected soil samples during Phase II site assessment activities indicated a TOC range from 1,700 to 14,000 milligrams per kilogram (mg/kg) in the upper clay zone and a range from 93 to 3,500 mg/kg in the uppermost sand zone. These concentrations indicate a relatively high sorptive capacity for the upper clay zone. While the lithologic features described above will tend to allow SVE to remove the majority of the contaminant relatively quickly, the sorptive capacity of the clay would tend to decrease the mobility of the remaining contaminant.

3.0 TECHNICAL APPROACH

3.1 Interim Remedial Action Goals

The general goal of the remediation work presented herein is to remove a maximum amount of halogenated VOCs from vadose zone soils in the three target areas as quickly and as cost effectively as is possible.

The primary technical goal is to select the best feasible technology presently available to remove halogenated VOCs and use that technology to its practical and economic limit. We propose that remediation of vadose soils in each subarea be discontinued when the following conditions have been met:

1. When the graph of extracted halogenated VOC concentration versus time becomes asymptotic. Because treatment in each area will be alternated as part of the operation and maintenance plan, we believe the most appropriate measure of the concentration decline curve should be the plot of the restart halogenated VOC concentrations versus time. An example concentration decline plot is presented on Plate 2.
2. When analytical results from confirmation samples indicate that a significant and consistent decline in soil halogenated VOC concentrations has resulted from the remedial action.

The remedial action described herein is intended to be implemented in a phased approach. The initial phase is intended to quickly remediate the subareas indicating the highest concentrations of reported halogenated VOCs. When the remedial goals discussed above have been achieved at any given subarea, the ongoing operational data review and evaluation of confirmation data will indicate the necessity to expand the system or target a new subarea.

3.2 Remedial Alternatives

The principal remediation alternatives that were considered are:

- Excavation of contaminated soils (upper clay zone) to a depth of 15 feet bgs in the three affected areas (North, Southwest, Southeast, as shown on Plates 3, 4, and 5, respectively), with transport offsite for disposal.

- Installation of upper clay zone and uppermost sand zone vapor extraction wells and/or trenches and installation of vapor extraction piping and collection manifolds in the three main affected areas. One of the three treatment technologies described below, or a combination of these technologies, would be used to alternately treat each of the selected subareas, one at a time, thus allowing halogenated VOC concentrations to equilibrate between treatment periods. It is anticipated that this approach will help maximize the total mass of halogenated VOCs removed per unit time. The three vapor extraction technologies considered are:
 1. Use of a trailer-mounted vapor refrigeration/condensation (R/C) equipment similar to that used during soil-vapor extraction testing conducted as part of the Phase II site assessment (HLA, 1993d). This system produces DNAPL and water condensate that must be recycled or disposed of offsite.
 2. Design skid-mounted SVE equipment incorporating a 5000-lb granular activated carbon (GAC) vessel that is regenerated onsite using existing, subcontracted, truck-mounted equipment. This process uses GAC vessels similar to those conventionally used to adsorb VOCs. Once the GAC reaches its adsorption limit, heated nitrogen and R/C equipment are used to remove the halogenated VOCs from the GAC, producing DNAPL and water that must be recycled or disposed of offsite.
 3. Design skid-mounted SVE equipment incorporating two conventional 1,200-lb GAC vessels. Once the GAC in the primary vessel reaches its adsorption limit, it is removed and replaced with fresh GAC. The flow direction through the vessels is then reversed, with the new GAC acting as the secondary, or scrubbing, unit. The expended GAC is transported offsite for regeneration.

3.3 Cost and Technical Comparison of the Alternatives

A planning-level cost estimate (PLCE) has been prepared to identify the main technical components and to compare the relative order-of-magnitude costs of these alternatives. A key assumption is that SVE can adequately remove halogenated VOCs from the clayey soils as indicated in the pilot SVE test (HLA, 1993d). The main conclusions that can be drawn from the PLCE are:

- The cost of excavation and offsite disposal or treatment of soil is approximately one order of magnitude higher than the well installation and SVE treatment options.
- The costs of the three SVE treatment options, excluding well installation costs, are within approximately 10 percent of each other for large-scale remediation. For smaller scale remediation, the trailer-mounted vapor R/C approach is most costly; the conventional GAC approach is next in cost, and the onsite GAC regeneration appears to be least costly.

- The trailer-mounted R/C approach rental costs are structured in tiers, with different influent concentrations determining pricing per unit time. This approach is price competitive with GAC alternatives at high and intermediate halogenated VOC concentrations, but at lower concentrations (for example at below 100 parts per million by volume) the relatively high energy consumption cost makes the R/C approach less economical. The costs of the two GAC-based alternatives are more directly related to the total mass of halogenated VOCs being removed and are more costly at higher influent concentrations. Therefore, a combination of technologies, employed in a modular fashion, appears to be the most cost-effective approach to long-term soil remediation.

3.4 Proposed Combination of Alternatives

In order to best take advantage of the individual cost effectiveness of the different SVE approaches under different extracted vapor concentration conditions, we propose the following combination of technical approaches to SVE remediation:

- Install either approximately seven SVE wells or horizontal vapor collection trenches in the upper clay zone and three SVE wells in the uppermost sand zone in each area. Well and/or trench spacing will be determined based on the results of the pilot testing performed during Phase II site assessment activities.
- Install approximately eight temporary soil-gas monitoring probes around the well and/or trench area in each target area.
- Install piping manifolds connecting the SVE wells and/or trenches.
- Operate the trailer-mounted R/C equipment in approximately 4-day periods at each affected area, alternating between the three areas for 4 weeks, or until extracted vapor concentrations drop to levels that make one of the GAC-based technologies more economical.
- Design and install an onsite regenerable GAC system or a conventional system that can be used to alternately treat soils in the three main affected areas until the remediation goals described above are achieved.

3.5 VES Conceptual Design

A trailer-mounted system will use a positive-displacement vacuum blower to apply a negative pressure (vacuum) to the vapor extraction wells and/or trenches and draw soil vapor into the wells. The soil vapor will then be passed through a refrigeration/condensation (R/C) unit to remove the halogenated VOCs from the vapor stream prior to discharge to the atmosphere.

When the concentration of halogenated VOCs in the airstream is reduced, GAC vessels will be employed to more cost-effectively remove halogenated VOCs from the extracted vapor stream.

The proposed treatment system will be used to alternately treat soils in the three areas to be remediated. The piping and electrical service will be installed in manner such that soils in the three target areas can be treated in alternation.

The VES, associated pipe manifolding from the wells, and electrical service panels will be contained in a secure fenced area(s). Piping manifold and fence locations will be chosen so as to minimize the impacts of construction and facility operations. If trenches are used, excavated soil may be placed in a contained treatment pile connected to the VE system.

The treatment compound(s) will have a 6-foot chain-link fence to secure the equipment. The fence will be constructed with swinging gates forming one side to facilitate the removal, installation, and GAC regeneration modular vapor extraction equipment. Reflective markings will be placed at the perimeter of the fencing to increase the visibility of the compound at night and reduce the potential for accidents. Warning signs will be placed on the fence to identify the compounds being treated within, and the access area of each compound will be designated a no parking zone.

4.0 REMEDIAL ACTION

4.1 Utility Clearance

To help ensure that underground piping, utilities, and obstructions are not encountered during drilling activities, HLA will:

- Based on the proposed vapor extraction well and/or trenches and temporary probe locations, review available maps and records provided by UTM for known subsurface obstructions;
- Mark locations of wells and/or trenches with representatives of UTM and relocate as necessary;
- Notify Underground Service Alert as required by law;
- Conduct a geophysical clearance survey and compare the results to available maps; and
- Hand auger the first 5 feet at each boring location and excavate by hand the leading edge of trenching.

4.2 Vapor Extraction Well and/or Trenches Installation

Ten-inch diameter soil borings will be drilled to a depth of approximately 15 feet bgs in the upper clay zone, and eight soil borings will be drilled to approximately 25 feet bgs in the uppermost sand zone with a truck-mounted hollow-stem auger drilling rig. An HLA geologist will supervise drilling, soil sampling, and well installation. Soil cuttings and samples will be monitored for organic vapors using a photo-ionization detector (PID). The PID will be calibrated daily to a hexane standard. Soil samples will be logged using the Unified Soil Classification System. Soil samples will be collected at 5-foot intervals. Samples may be selected for submittal to Del Mar Analytical, Irvine, California, for analysis of halogenated VOCs using EPA Method 8010. The samples submitted for analysis will be selected based on field screening and visual observation.

The borings will be converted to 4-inch diameter vapor extraction wells. The wells will be constructed of Schedule 40, flush-threaded, 0.020-inch slot PVC casing from approximately 3 feet to 14 feet bgs in the upper clay zone and from approximately 16 to 25 feet bgs in the

uppermost sand. Blank Schedule 40 PVC casing will be installed above the screened section. No. 3 Monterey sand will be used as a filter pack in the annular space surrounding the casing to approximately 1 foot above the screened section. An approximately 1.5 foot thick hydrated bentonite seal will be placed above the filter pack in the upper clay zone wells. This seal will be approximately 5 feet thick in the uppermost sand zone wells. A bentonite-cement grout mixture will be used to seal each boring above the hydrated bentonite. The wellheads will remain uncompleted pending installation of the SVE piping and then completed with flush-mount, traffic-rated well boxes. Typical well completion details are presented on Plate 7.

If vapor extraction trenches are employed, they will be excavated to approximately 8 feet bgs in the upper clay zone and constructed as indicated on Plate 8.

Soil cuttings and decontamination fluids will be placed in appropriate containers and stored onsite pending receipt of analytical results for subsequent offsite disposal.

4.3 Temporary Soil Vapor/Vacuum Piezometer Installation

Approximately eight temporary soil vapor/vacuum piezometers will be installed at each of the subareas. The piezometers will be installed by pushing a standard 1/2-inch-diameter soil-gas probe to the target depth. A 1/8-inch-diameter polypropylene tube will be installed in the center of the probe. As the steel probe is carefully withdrawn, filter sand will be placed in the probe using a technique similar to that used to build the vapor extraction wells within the hollow stem augers. The filter sand will be placed approximately 6 inches above the bottom of the tube, and the remainder of the tube will be filled with hydrated bentonite. Each tube will be immediately capped following installation.

4.4 VES Construction and Installation

Construction activities will include trenching and installation of subgrade PVC piping from the wells; assembly of a collection, valving, and sampling manifold, installation of electrical service (if portable generators are not used), and installation and marking of the fenced

compounds. Following the trailer-mounted R/C unit operation, piping to connect the three target areas may be installed, and GAC-based VES equipment will be installed.

4.5 Permitting

Permitting approvals will be required from various regulatory agencies. The lead agency overseeing the remediation progress will be the RWQCB. The RWQCB will review this IRAP as a workplan for remediation activities onsite, and upon approval, the IRAP will guide future activities. Other agencies from which permits and/or approval will be required include:

- South Coast Air Quality Management District (SCAQMD)
- Local Building and Safety Department
- Local Fire Department

During the initial phase of remediation, the trailer-mounted R/C unit will be used to remediate soils. This unit is permitted by the SCAQMD for use in various locations for up to 90 days. During this 90-day period, HLA can apply for a fixed location permit to operate GAC-based equipment past the 90-day period. The fixed location permit will require approximately 6 weeks for approval and is expected to be obtained prior to the expiration of the various locations permit.

4.6 Implementation

4.6.1 System Startup

Once piping installation has been completed, the trailer-mounted R/C system should require relatively little time to become fully operational. We anticipate that approximately 1 day will be required for startup at each area.

Approximately 1 week will be required for startup at each area for the GAC-based system.

During this period, the following work will be performed:

- Troubleshooting of system during startup,
- Final equipment and piping modifications,
- Collection of baseline data, and
- Development of initial operation parameters and valve/control settings.

The SCAQMD permit for the fixed GAC-based system will likely require 2 weeks of daily monitoring and one-time influent and effluent sampling at startup. The samples will be analyzed for halogenated VOCs using EPA Method TO14 collected in Tedlar bags or Summa canisters. All samples will be submitted to a State of California-certified laboratory according to chain-of-custody protocol.

During the first 6 weeks of system startup and operation, HLA and/or our subcontractors will monitor the VES daily to ensure that the equipment is operating correctly, to collect operations and concentration information, to compare operating data to the general operational plan, and to adjust and optimize the system as necessary.

4.6.2 Operation and Maintenance

At each subarea, vapors will be withdrawn from the soil for a specified number of days and then will be turned off for a specified number of days (for example, 10 days on, 20 days off) in each of the three target areas to allow soil conditions (especially in the fine-grained soils) to return to equilibrium. We believe that alternating treatment at each of the areas should maximize overall halogenated VOC mass removal per unit time.

Air sampling will be conducted in accordance with SCAQMD permit requirements. On each site visit, the influent and effluent concentrations of the VES will be measured using a PID. Influent vapor samples will also be periodically collected to evaluate the concentrations of halogenated VOCs being removed from the soil.

Based on operational results, different combinations of wells and/or trenches may be used for vapor extraction and passive air inlet to help maximize total halogenated VOC mass recovery.

4.6.3 Reporting

HLA will compile and evaluate the VES operational data and will issue draft quarterly reports for review by UTM. The reports will summarize field activities, discuss conditions encountered during remediation, present key operational parameters, and calculate mass removal rates. After UTM's review, final quarterly reports will be submitted to the RWQCB, if required.

During VES operations, HLA will assess the monitoring data for progress of remediation. Once the extracted halogenated VOC concentrations have declined sufficiently, HLA will collect confirmation samples to assess the type and concentration of halogenated VOCs remaining in the soil. Depending on the analytical results obtained, HLA may request RWQCB approval to cease remedial operations, may continue to operate the VES, or may modify the remedial operation.

4.7 Interim Remedial Action Schedule

This IRAP can be submitted to the RWQCB in early February 1994. The RWQCB is estimated to require 4 weeks to review, comment, and issue approval. An approximate schedule of activities to be performed after RWQCB approval is presented on Plate 6.

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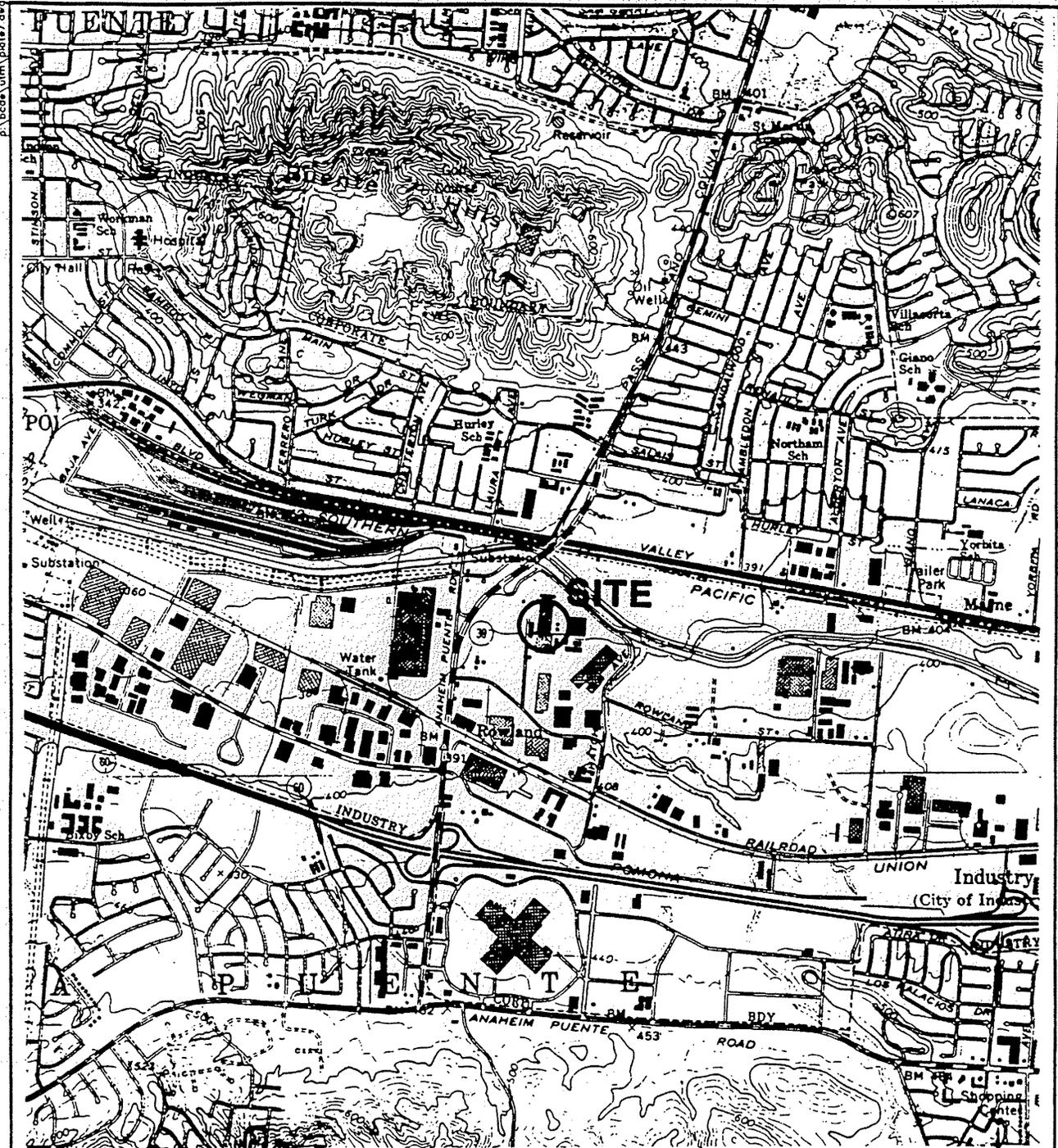
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ILLUSTRATIONS

UTM 004579



Reference: USGS 7.5-minute quadrangles, Baldwin Park and La Habra, California (photorevised 1981)

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Engineering and Environmental Services

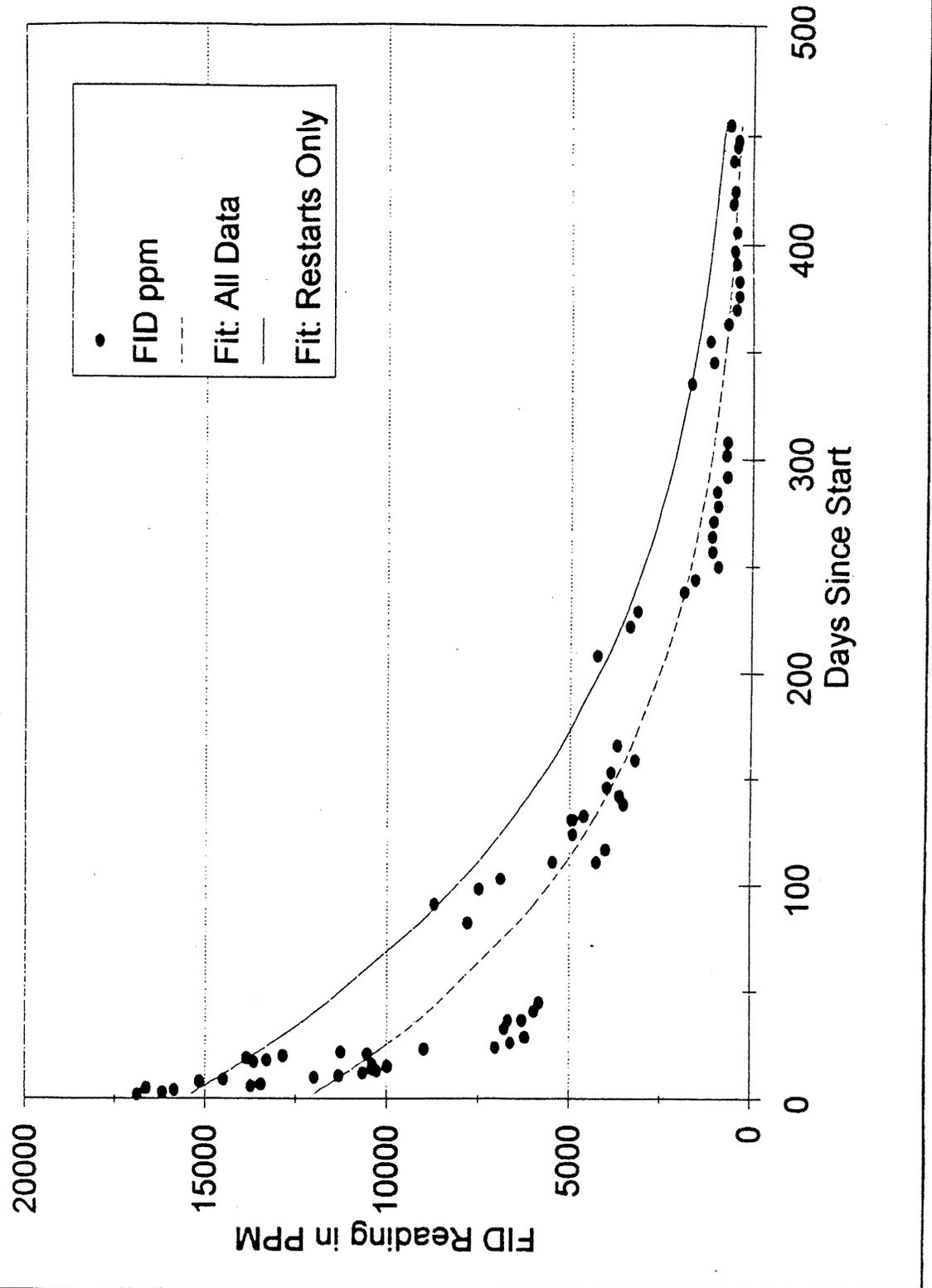
VICINITY MAP
Utility Trailer Manufacturing Company
City of Industry, California

1

DRAWN	PROJECT-TASK NUMBER	APPROVED	DATE	REVISED	DATE
JTL	26961-2	BCD	11/93		

UTM 004580

Vapor Concentration vs. Time with Exponential Best-Fits



HLA Harding Lawson Associates
Engineers and Geoscientists

**TYPICAL CONCENTRATION DECLINE PILOT
SOIL VAPOR EXTRACTION SYSTEM INFLUENT**
Utility Trailer Manufacturing Company
City of Industry, California

PLATE
2

DRAWN
khw

JOB NUMBER
26961-2

APPROVED

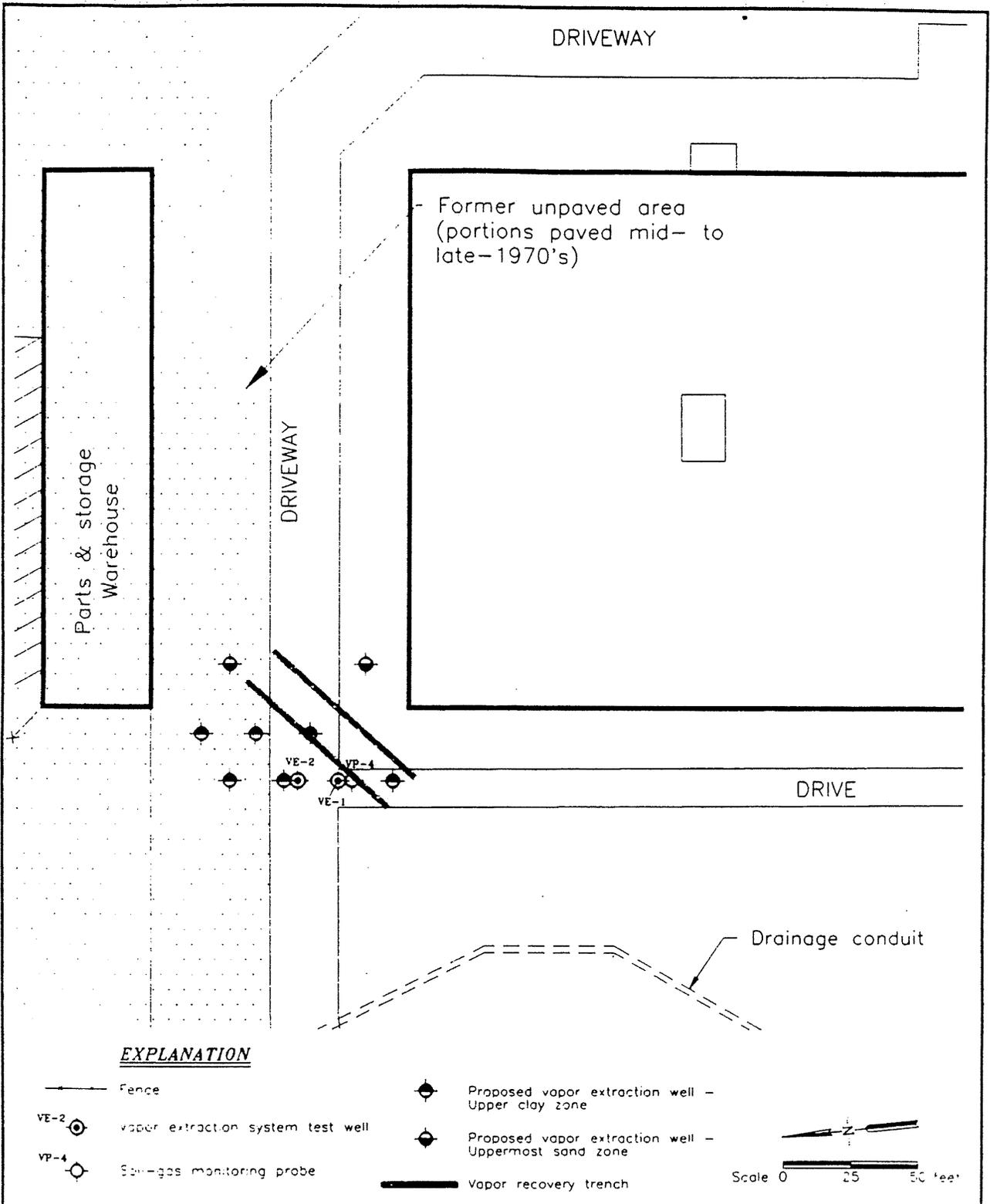
DATE
1/04

REVISED

DATE

UTM 004581

USER 1 PLOT 1 * 50
 HOI: 26961\2\19451



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 Engineering and
 Environmental Services

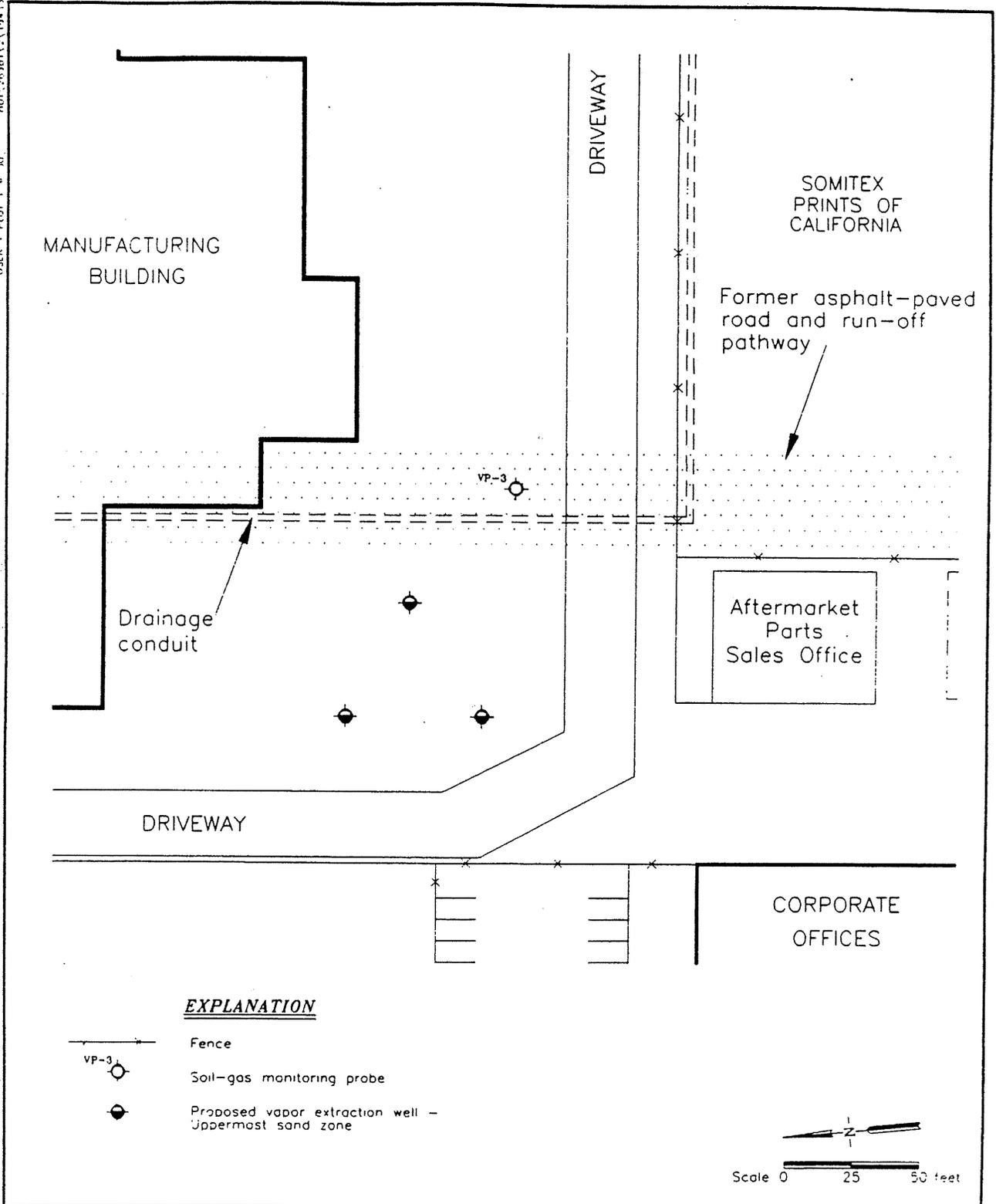
PROPOSED VAPOR EXTRACTION WELLS
NORTH AREA
 Utility Trailer Manufacturing Company
 City of Industry, California

PLATE
3

DRAWN	PROJECT-TASK NUMBER	APPROVED	DATE	REVISED	DATE
HLA	26961-2		2/94		

UTM 004582

USER 1 PLOT 1 = 50
HOT 26961-2 194.3



EXPLANATION

- Fence
- VP-3
Soil-gas monitoring probe
- Proposed vapor extraction well -
Uppermost sand zone

HLA Harding Lawson Associates
Engineering and
Environmental Services

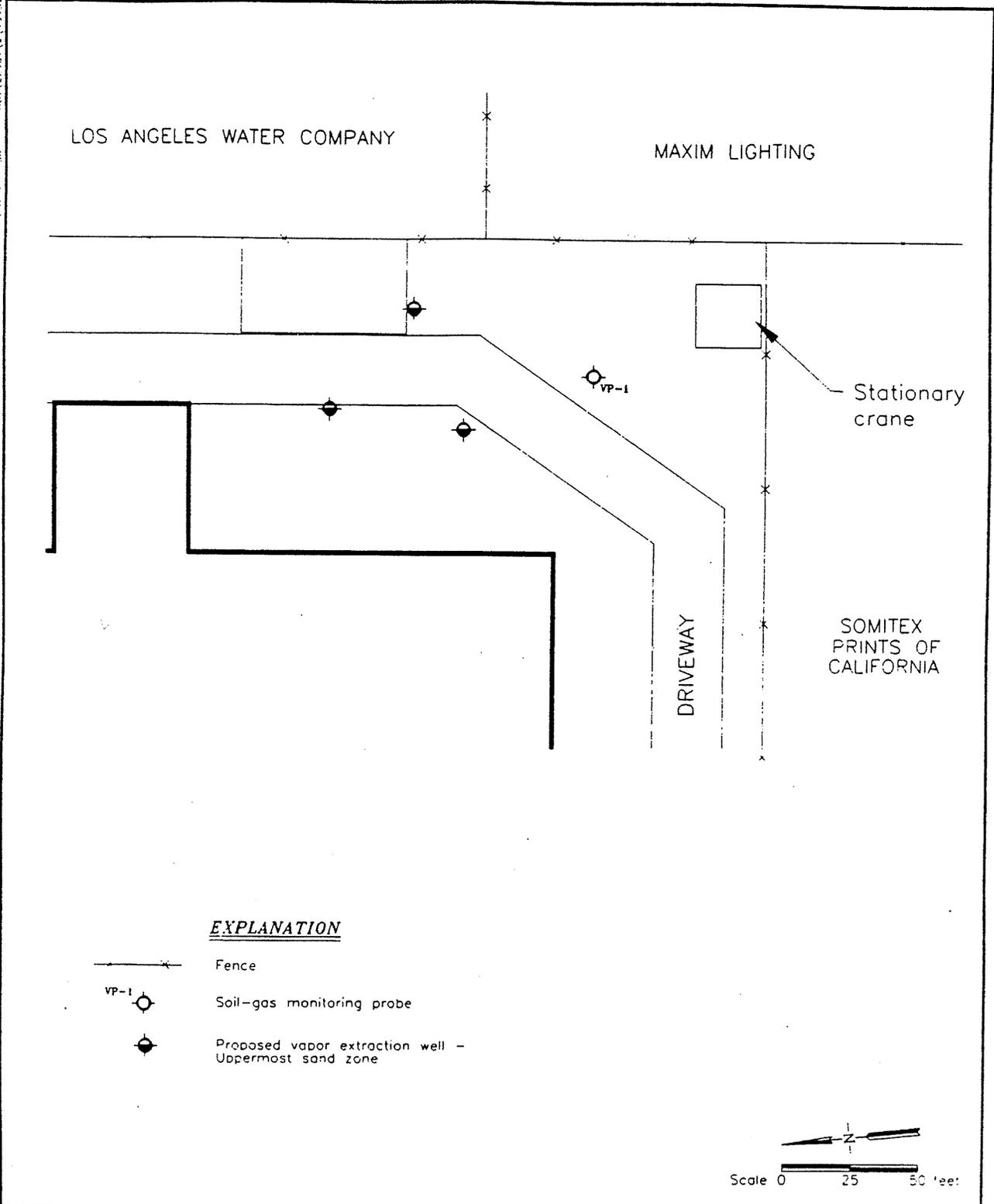
PROPOSED VAPOR EXTRACTION WELLS
SOUTHWEST AREA
Utility Trailer Manufacturing Company
City of Industry, California

PLATE
4

DRAWN JTC	PROJECT-TASK NUMBER 26961-2	APPROVED	DATE 2/94	REVISED	DATE
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UTM 004583

HSR 1 PLOT 1 x 50 H0126961A2/1945



EXPLANATION

- Fence
- Soil-gas monitoring probe
- Proposed vapor extraction well - Uppermost sand zone

HLA Harding Lawson Associates
 Engineering and
 Environmental Services

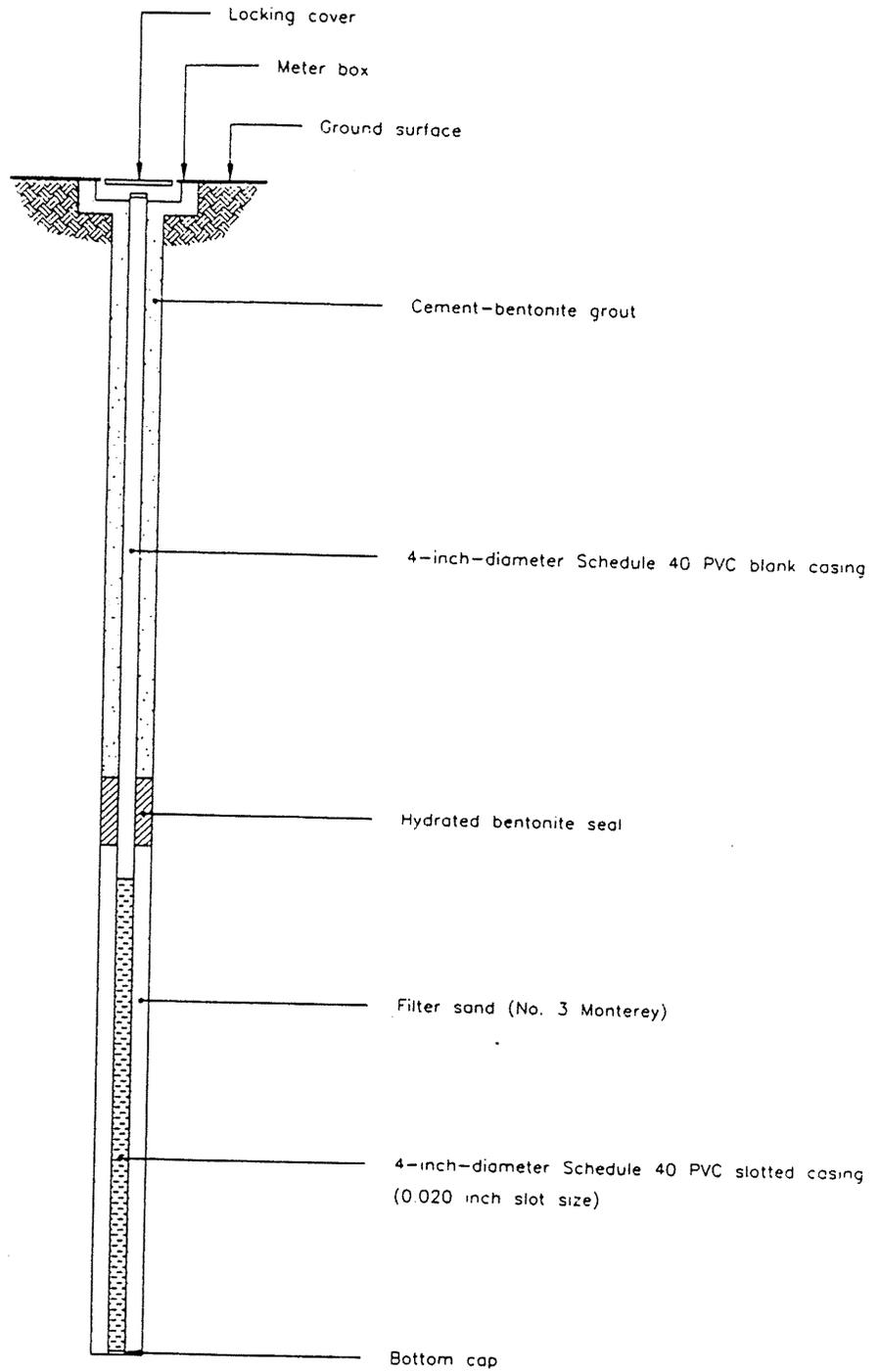
**PROPOSED VAPOR EXTRACTION WELLS
 SOUTHEAST AREA**
 Utility Trailer Manufacturing Company
 City of Industry, California

PLATE
5

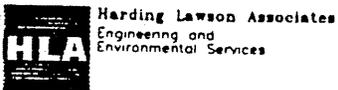
DRAWN	PROJECT - ASH NUMBER	APPROVED	DATE	REVISED	DATE
	26961-2		2/94		

UTM 004584

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Not to scale



WELL COMPLETION DETAILS
VAPOR EXTRACTION WELL
 Utility Trailer Manufacturing Company
 City of Industry, California

PLATE 7

DRAWN
bcde

PROJECT-TASK NUMBER
26961-2

APPROVED

DATE

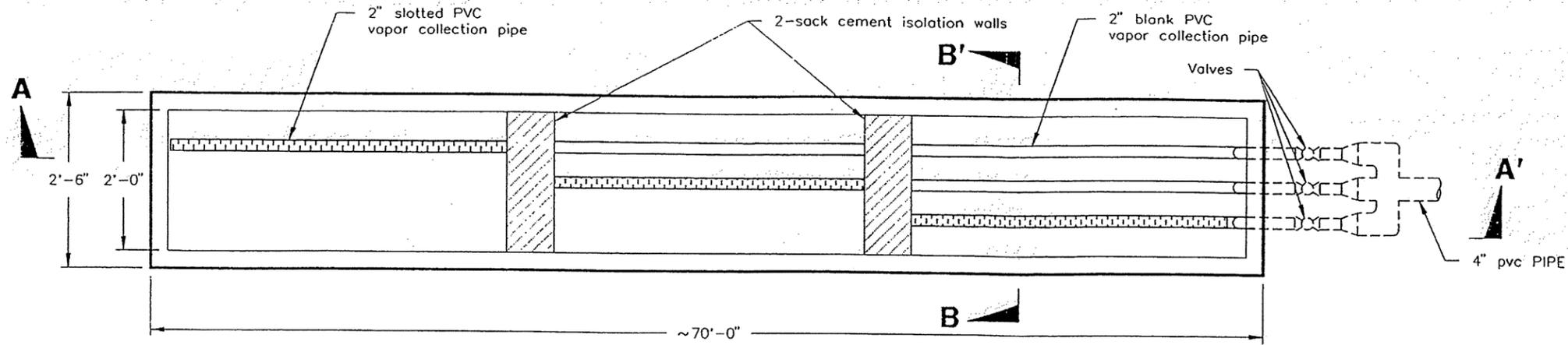
2/94

REVISED

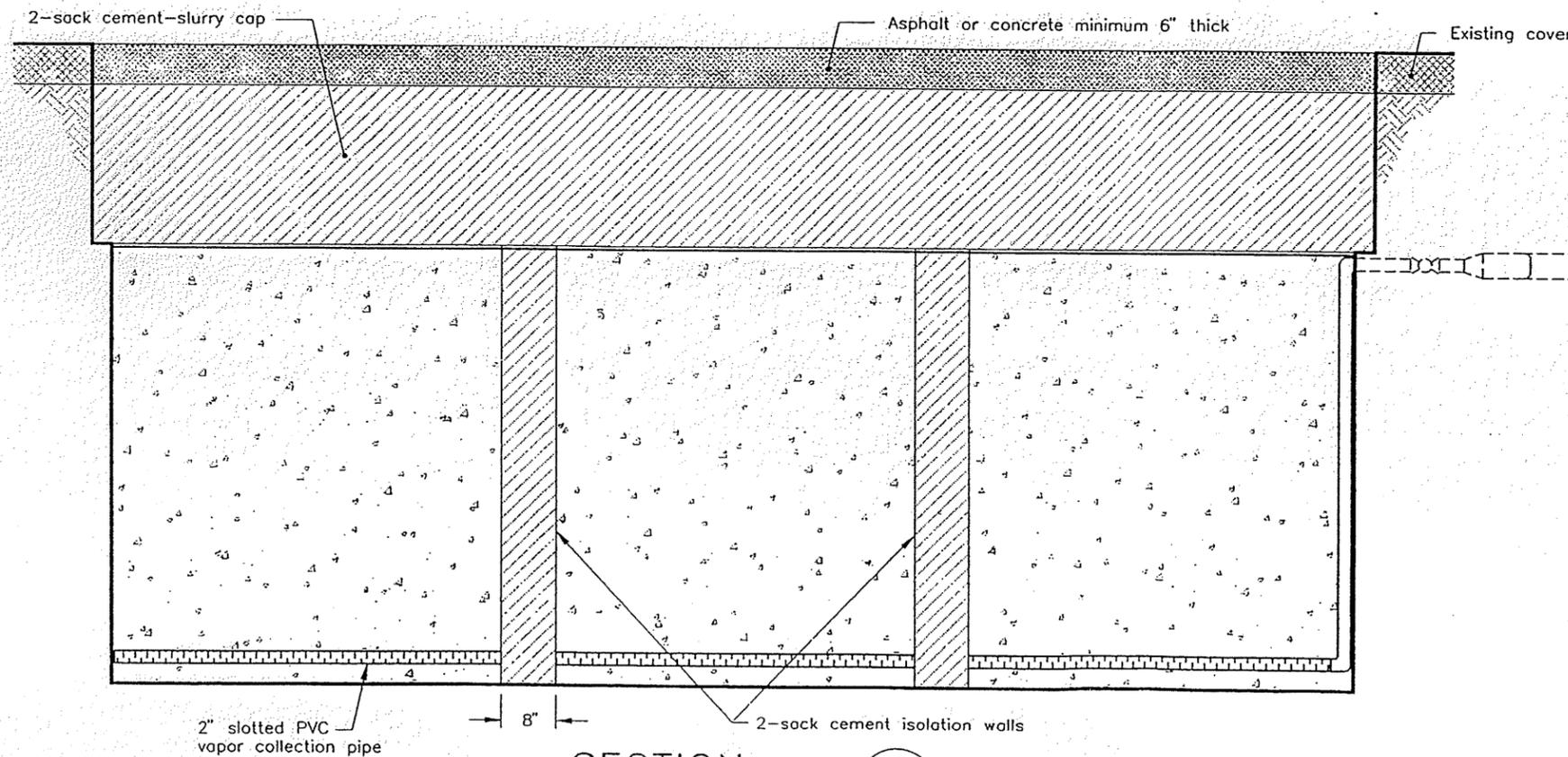
DATE

UTM 004586

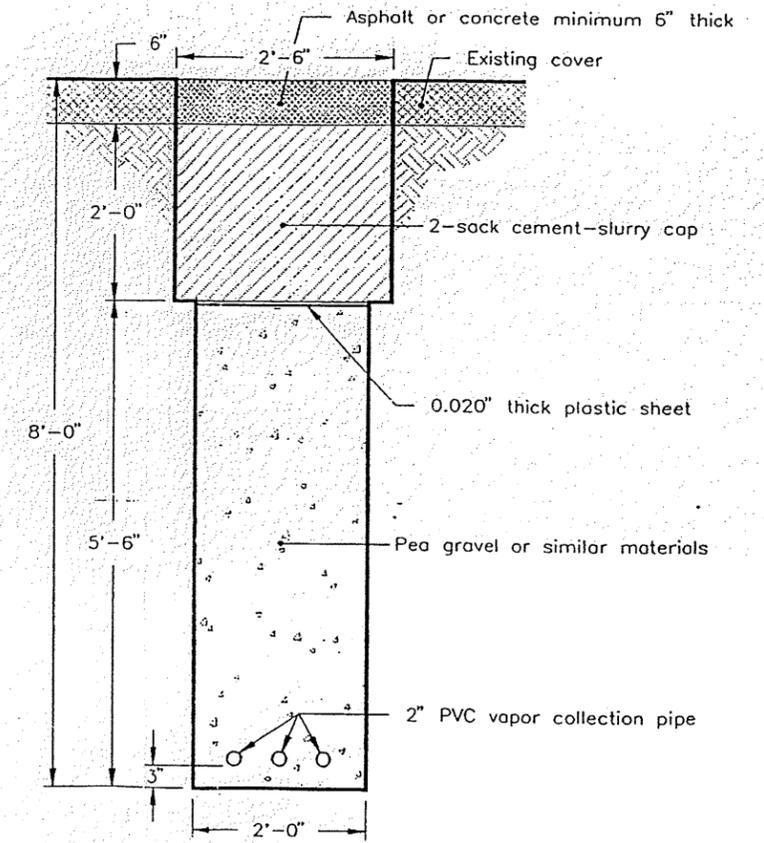
HDV 26961 \ V. 2341



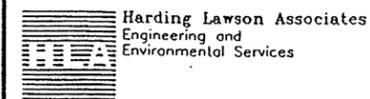
PLAN VIEW
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SECTION A-A'
Not to scale



SECTION B-B'
Not to scale



DRAWN
JTL

PROJECT-TASK NUMBER
26961-2

APPROVED

DATE
2/94

REVISED

DATE

VAPOR EXTRACTION TRENCH DETAILS
Utility Trailer Manufacturing Company
City of Industry, California

PLATE

8

UTM 004587

DISTRIBUTION (DRAFT)

Draft Interim Remedial Action Plan
Soil Vapor Extraction
Utility Trailer Manufacturing Company
17300 East Chestnut Street
City of Industry, California

February 10, 1994

Copy 1: Mr. Robert Griffis
Utility Trailer Manufacturing Company
17295 East Railroad Street
City of Industry, California 91749

Copy 2: Job File

Quality Control Reviewer

William S. Sedlak
Associate Engineer